

MSMF GATE CENTRE

Subject: Control Systems

Test 4: Root Locus Diagram (RLD) & Frequency response Analysis

(Solutions)

1. **Ans: (c)**

Sol:

RLD starts at a pole ($k = 0$) and terminates at a zero ($k = \infty$) of the OLTF $G(S)H(S)$

2. **Ans: (b)**

Sol:

$k = \infty$ RLD ends at open loop zeros, they are the closed loop poles for $k = \infty$.
 $\therefore j2, -j2, \infty$ are the closed loop poles.

3. **Ans: (d)**

Sol:

Centroid always lies on the real axis
 Centroid $(\sigma) =$

$$\frac{\sum \text{real parts of poles of } G(s)H(s) - \sum \text{real parts of zero of } G(s)H(s)}{P - Z}$$

which gives real quantity

4. **Ans: (d)**

Sol:

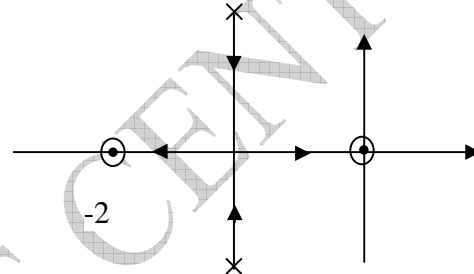
Break away point can lie anywhere in the s-plane

E.g. $G(s)H(s) = \frac{K}{(s^2 + 2s + 2)^2}$ Break

away points are $-2 \pm j2$

5. **Ans: (a)**

Sol:



It is clear from the RLD at $S = -2$ arrival is 0^0 .

6. **Ans: (c)**

Sol:

$$\text{OLTF} = \frac{K}{4 - S} = \frac{-K}{(S - 4)}$$

(or) Characteristics Equation

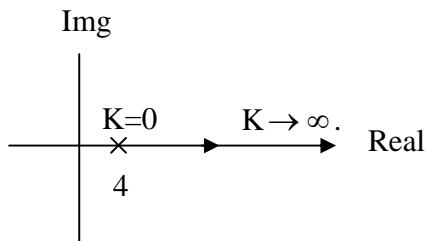
$$1 + \frac{K}{4 - S} = 0$$

$$4 - S + K = 0$$

$$S = K + 4$$

As K increases root moves towards right side of s-plane

\therefore RLD is



$$OLTF = \frac{CLTF}{1 - CLTF} = \frac{\frac{k}{s+2+k}}{1 - \frac{k}{s+2+k}} = \frac{k}{s+2}$$

$$K|_{s=-6} = \frac{1}{\left(\frac{1}{s+2}\right)}$$

7. **Ans: (b)**

Sol:

It is clear from the RLD that the system is stable for only certain positive values of K

from '0' the only answer is $0 < k < 10$

$$K = |s+2|_{s=-6}$$

$$K = |-6+2| = 4$$

$$K = 4$$

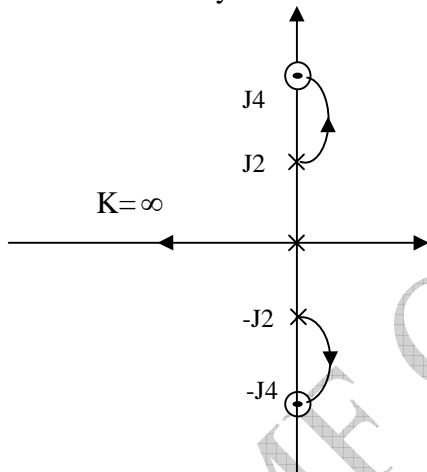
(Or) **Method 2**

Characteristic equation is $s+2+k=0$, $s=-2$ will give $k=4$

8. **Ans: (b)**

Sol:

RLD of the system is shown in fig below



It is clear from the RLD $S_1 = j3$ is not on the RLD, but $S_2 = -5$ is on the RLD

Method II

One may use the angle condition to verify the same.

10. **Ans: (c)**

Sol: It is clear from the given RLD that the option in (a) (b) (d) are not at all valid \therefore the only option is (c) which is correct.

11. **Ans: (d)**

Sol:

Characteristic equation is $1 + \frac{K(S+4)}{S(S^2+6S+13)}$

$$S(S^2+6S+13)$$

$$S^3 + 6S^2 + 13S + KS + 4K = 0$$

$$S^3 + 6S^2 + (13+K)S + 4K = 0$$

$$S^3 \quad \left| \quad \begin{array}{l} 1 \qquad \qquad \qquad 13+K \\ 6 \qquad \qquad \qquad 4K \\ \frac{6(13+K)-4K}{6} \end{array} \right.$$

$$S^2 \quad \left| \quad \begin{array}{l} 6 \\ 4K \end{array} \right.$$

$$S^1 \quad \left| \quad \frac{6(13+K)-4K}{6} \right.$$

$$S^0 \quad \left| \quad 4K \right.$$

$$S^0 \quad \left| \quad 4K \right.$$

$$S^1 \text{ row} = 0, \quad \frac{6(13+K)-4K}{6} = 0$$

$$(13)(6) + 6K - 4K = 0$$

$$2K = (-13)(6)$$

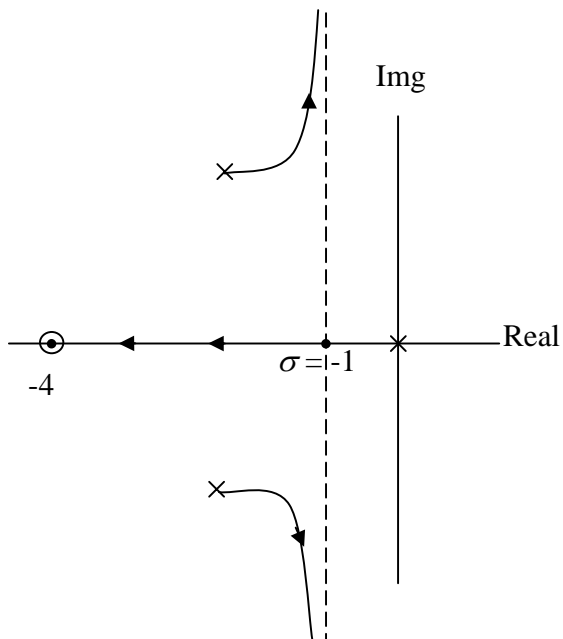
$$K = -Ve$$

\therefore For Positive values of 'K' $0 < k < \infty$, the RLD it will not intersect.

The RLD is given below

9. **Ans: (a)** (correction in the question)

Sol:



It is clear that it will not intersect the $j\omega$ axis.

12. **Ans: (a)**

Sol:

$$1 + G(S)H(S) = S(S+2) + K(S+3) = 0$$

$$1 + \frac{K(S+3)}{S(S+2)} = 0$$

$$\therefore G(S)H(S) = \frac{K(S+3)}{S(S+2)}$$

$$\frac{d}{ds} \left[\frac{S+3}{S(S+2)} \right] = 0$$

$$S^2 + 6s + 6 = 0$$

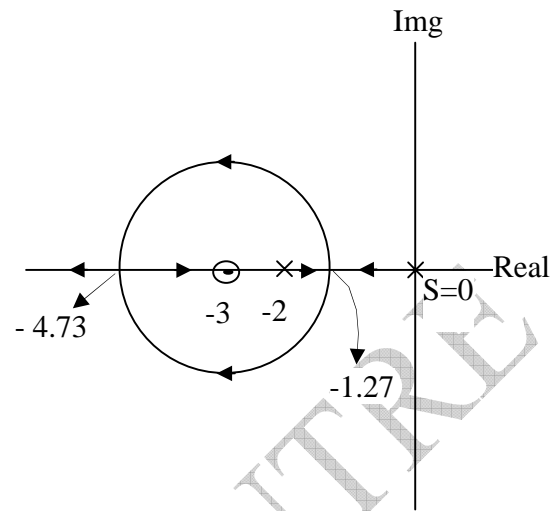
$$\text{Roots are, } -3 \pm \sqrt{3}$$

i.e. $-1.27, -4.73$, are the break away points.

13. **Ans: (b)**

Sol:

The RLD is given below



The diameter of the circle is the distance between the break away points
i.e. $(4.73 - 1.27) = 3.46$

14. **Ans: (b)**

Sol:

$$\begin{array}{l|ll} S^3 & 1 & 16 \\ S^2 & 30 & 16K \\ S^1 & \frac{30(16) - 16K}{30} & \\ S^0 & 16K & \end{array}$$

$$S^1 \text{ row} = 0$$

$$30(16) - 16K = 0$$

$$K = 30$$

$$AE = 30S^2 + 16K = 0$$

$$30S^2 + 16(30) = 0$$

$$S = \pm j4$$

\therefore RLD intersection at $S = \pm j4$

15. **Ans: (b)**

Sol:

$$1 + G(S)H(S) = 0$$

$$S^3 + 30S^2 + 16S + 16K = 0$$

$$1 + \frac{16K}{S^3 + 30S^2 + 16S} = 0$$

$$G(S)H(S) = \frac{16K}{S(S^2 + 30S + 16)}$$

$$P = 3, Z = 0$$

$$\therefore \text{No of asymptotes} = |P-Z| \\ = |3-0| = 3$$

16. Ans: (d)

Sol:

Frequency response is the steady state output of a system to the sinusoidal input.

17. Ans: (c)

Sol:

Eg: Transportation lag = e^{-sT_d}
It introduces the negative phase, hence Phase and Gain margins of the system decreases

\therefore Stability decreases.

18. Ans: (b)

Sol:

$$GM = \frac{1}{|G(j\omega_{pc})H(j\omega_{pc})|}$$

It is clear from the expression the gain is decreased then GM increases, hence if the gain is made half, GM increase by '2'.

19. Ans: (a)

Sol:

$$f = 0.1591 \text{ Hz}$$

$$\omega = 2\pi f = 2\pi(0.1591) = 1 \text{ rad/sec}$$

$$\left| \frac{1}{(j\omega)^2 + j\omega + 1} \right|_{\omega=1} = \left| \frac{1}{\sqrt{(1-\omega^2)^2 + \omega^2}} \right|_{\omega=1} = 1$$

$$\text{(or) } 20\log 1 = 0 \text{ dB}$$

20. Ans: (b)

Sol:

If peak overshoot is zero, implies that damping ratio, $\xi \geq 1$

$$\text{Resonant peak for } \xi \geq \frac{1}{\sqrt{2}} \text{ is '1'}$$

21. Ans: (b)

Sol:

Stable range of k is $0 < k < 20$

The value of k for marginal stability

$$GM = \frac{\text{Required value of K}}{\text{Required value of K}}$$

$$\frac{20}{10} = 2$$

$$GM = \frac{20}{10} = 2$$

$$\text{(or) GM in dB} = 20\log 2 = 6\text{dB}$$

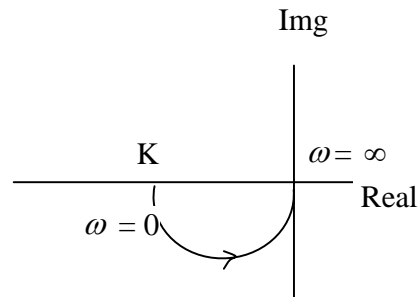
22. Ans: (c)

Sol:

$$\text{Eg. OLTF} = \frac{K}{S-2}$$

$$= \frac{K}{j\omega-2} = \frac{K}{\sqrt{\omega^2+4} - (180-\tan^{-1} \frac{\omega}{2})}$$

The Polar plot is



23. Ans: (c)

Sol:

Eg let us consider a system with $G(S)H(S) = \frac{K}{S(S+2)}$

$$\frac{K}{S(S+2)}$$

This system is stable for $0 < K < \infty$

24. Ans: (d)

Sol:

System is marginally stable

$$\therefore GM = 1 \text{ (or) } 0 \text{ dB}$$

$$\& PM = 0^\circ$$

$$K = 20$$

25. **Ans: (a)**

Sol:

It is a polar plot of type '0' system

∴ Option "a" is correct

$$\begin{aligned} \therefore \text{TF } G(S)H(S) &= \frac{20S}{(1+S)(1+S \cdot \frac{1}{10})} \\ &= \frac{20S}{(1+S)(1+0.1S)} \end{aligned}$$

26. **Ans: (c)**

Sol:

G(S)H(S) has a pole at the origin and poles on the jω axis

∴ option 'c' is correct

28. **Ans: (b)**

Sol:

$$\begin{aligned} \text{CLTF} &= \frac{G(S)}{1+G(S)H(S)} \\ &= \frac{20S}{(1+S)(1+0.1S)+20S} \end{aligned}$$

$$|\text{CLTF}|_{\omega=0} = 0$$

27. **Ans: (d)**

Sol:

Corner frequencies are $\log \omega_1 = 0$

$$\omega_1 = 1$$

$$\frac{1}{\omega_1}$$

$$\therefore T_1 = \frac{1}{\omega_1}$$

and $\log \omega_2 = 1$

$$\omega_2 = 10$$

$$\frac{1}{\omega_2}$$

$$\therefore T_2 = \frac{1}{\omega_2}$$

The starting point frequency $\log \omega = -1$
 $\omega = 0.1$

29. **Ans: (d)**

Sol:

For $a > 1$, $(-1, j0)$ is enclosed once in the ccw direction

∴ $N = 1$, (from the plot)
& $P = 1$ (Given)

$$N = P - Z$$

$$Z = P - N$$

$$Z = 1 - 1 = 0$$

$$Z = 0 \text{ System is stable}$$

$$a > 1, \text{ hence } a = 1.5$$

Initial slope is 20 dB/dec hence portion of the TF $= G(S)H(S) = Ks$

At $\omega_1 = 1$ slope changes to '0' dB. i.e. -20 dB/dec is added to initial slope +20 dB/dec, implies there is a presence of real pole

Hence portion of the TF $G(S)H(S) =$

$$\frac{KS}{1+sT_1}$$

At $\omega_2 = 10$ slope become -20dB/dec implies another pole is added

$$\therefore \text{Total TF } G(S)H(S) =$$

$$\frac{Ks}{(1+sT_1)(1+sT_2)}$$

$$|K| + |S| = 6\text{dB} / \omega = 0.1$$

$$(20\log K + 20\log \omega)_{\omega=0.1} = 6\text{dB}$$

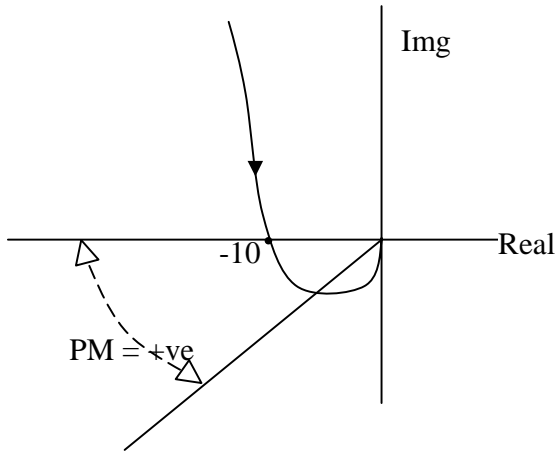
30. **Ans: (c)**

Sol:

For $a = 10$

PM is +Ve

$$\therefore \text{PM} = 45^\circ$$



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